



Theodore Wind Farm

Noise Impact Assessment

24 July 2024

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Abbreviations

AO	Acceptable Outcome of the State code 23
BESS	Battery Energy Storage System
EPA	Environment Protection Authority
Good Practice Guide	<i>Institute of Acoustics (UK) "A Good Practice Guide to the Application of ETSU-R-97 for the Assessment and Rating of Wind Turbine Noise"</i>
ISO 9613-2	<i>ISO 9613-2:1996 Acoustics – Attenuation of sound during propagation outdoors – Part 2: General method of calculation</i>
MVA	Megavolt Amperes
MW	Mega Watt
MWh	Mega Watt hour
OEM	Original Equipment Manufacturer
PO	Performance Outcome of the State code 23
Policy	<i>Environmental Protection (Noise) Policy 2019</i>
Project	Theodore Wind Farm
SARA	State Assessment and Referral Agency
Scheme	<i>Banana Shire Council Planning Scheme 2021</i>
State code 23	<i>State code 23: Wind farm development of the State Development Assessment Provisions, Version 3.0</i>
State code 23 guidance	<i>Planning guidance - State code 23: Wind farm development, February 2022</i>
TED	Theodore Energy Development Pty Ltd
WTG	Wind Turbine Generator

Glossary

A-weighting	A mathematical adjustment to the measured noise levels to represent the human response to sound. An <i>A-weighted noise level</i> is presented as dB(A)
Background creep	An increase in the total amount of background noise in the area from the introduction of new noise sources
Background noise level	Minimum ambient noise level, evaluated as the level exceeded for 90 per cent of 10-minute sample periods. Nomenclature for the background noise level is L_{A90}
Candidate WTG	A candidate WTG is used as an example to indicate the ability of the wind farm to comply with legislative requirements. Candidate WTGs are indicative of WTGs which might be procured at a future design and tender stage
Day	6.00 am to 10.00 pm

Decibels	The logarithmic unit of measurement to define the magnitude of a fluctuating air pressure wave. Presented as dB and used as the unit for <i>sound</i> or <i>noise level</i>
Deed of Release	Written agreement from non-host lot owners within 1500m of the nearest WTG
Equivalent noise level	The A-weighted noise level which is equivalent to a noise level which varies over time. Nomenclature for the <i>A-weighted equivalent noise level</i> is L_{Aeq}
Frequency	Frequency is the number of pressure fluctuation cycles per second of a sound wave. Measured in units of Hertz (Hz)
Host lot	A host lot is a sensitive land use which accommodates any part of a wind farm
Noise	An interchangeable term with sound but which is most often described as <i>unwanted sound</i> .
Non-host lot	A non-host lot is a sensitive land use no part of which is used for a wind farm
Night	10.00 pm to 6.00 am
Octave Band	The segregation of sound into discrete frequency components. For example, the 63 Hz <i>octave band</i> is a low frequency component of sound/noise, and the 2000 Hz <i>octave band</i> is a high frequency component of sound/noise. The one-third (or 1/3) octave is more finite segregation (1/3 rd) of each octave band
Sensitive land uses	Existing or approved sensitive land uses as identified in State code 23. This includes, amongst other things, dwellings, community and childcare facilities, health care facilities, schools and tourist parks
Sound	An activity or operation which generates a fluctuating air pressure wave. The ear drum can perceive both the frequency (pitch) and the magnitude (loudness) of the fluctuations to convert those waves to sound
Sound pressure level	The magnitude of sound (or noise) at a location. The sound pressure level can vary according to distance to the noise source, and operational, meteorological and topographical influences. The terms <i>Sound Pressure Level</i> and <i>Noise Level</i> are used interchangeably in this Noise Impact Assessment
Sound power level	The amount of sound energy an activity produces for a given operation. The sound power level is a constant value for a given activity. The sound power level is analogous to the power rating on a light globe (which remains constant), whereas the lighting level in a space (sound pressure level in this analogy) will be influenced by the distance from the globe, shielding and different locations within the space
Tonality	Noise containing a perceptible pitch component as objectively identified using a one-third octave band test as per State code 23 guidance
Warranted sound power level	The sound power level which the WTG supplier guarantees can be achieved inclusive of uncertainties

Introduction

Theodore Energy Development Pty Ltd (**TED**) is proposing to develop the Theodore Wind Farm (the **project**) in the Banana Shire Council local government area.

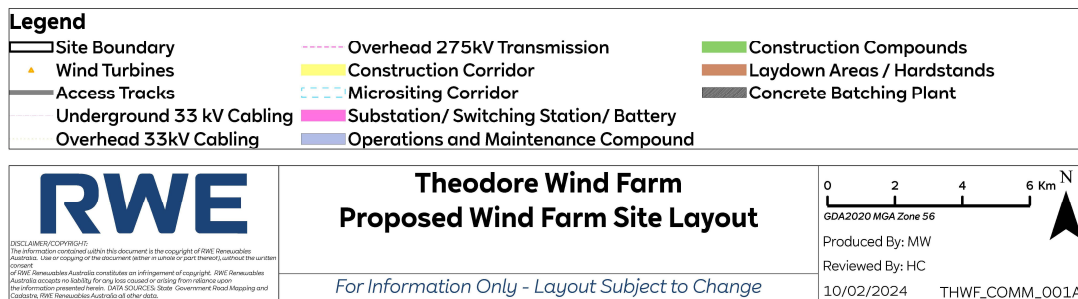
The project will be located approximately 30km east of the Theodore township and has the potential for up to 170 wind turbine generators (**WTGs**) each with a generating capacity in the order of 7.2 MW, four Battery Energy Storage Systems (**BESSs**) each with a capacity of 250 MW / 500 MWh, and associated transformers.

The candidate WTG for the project is the *Vestas V172-7.2MW* producing a total installed capacity of up to 1224 MW. The combined battery storage capacity will be up to 1000 MW / 2000 MWh.

State code 23: Wind farm development of the *State Development Assessment Provisions* provides requirements to protect the amenity of existing or approved sensitive land uses from acoustic impacts associated with the WTGs, and the *Environmental Protection (Noise) Policy 2019* provides a method of assessing adverse noise impacts from the BESSs and transformers.

The noise levels generated from renewable energy facilities are well understood and can be predicted. This noise impact assessment (the **assessment**) predicts the noise associated with the WTGs, BESSs, and transformers to ensure the acoustic amenity of the surrounding existing and approved sensitive land uses is not adversely affected by the project.

The layout for the project is shown in Figure 1 below.



Assessment Criteria

Banana Shire Council Planning Scheme 2021

The project is located within a *Rural Zone* of the *Banana Shire Council Planning Scheme 2021* (the **scheme**).

A renewable energy facility is categorised as an “Assessable Development” under the scheme.

In addition to the assessment requirements for wind farm developments by the State Assessment and Referral Agency (**SARA**), the scheme has the following provisions relating to noise from the ancillary infrastructure:

Performance Outcome PO5 (Amenity Section)

The acoustic objectives of the *Environmental Protection (Noise) Policy 2019* are maintained for the ongoing operation of the use.

Performance Outcome PO35 (Renewable energy facility Section)

Operations do not disturb the early morning or late evening amenity of the locality.

Environmental Protection (Noise) Policy 2019

Performance Outcome PO5 references the *Environmental Protection (Noise) Policy 2019* (the **Policy**).

The Policy provides a management hierarchy for managing noise. Where a noise source is located near a sensitive receptor, the noise must be minimised to ensure:

- a) the noise does not have any adverse effect, or potential adverse effect on an environmental value. For continuous noise sources, the “environmental value” is satisfied at residences by achieving the following noise levels:
 - 50 dB(A) outdoors during the daytime and evening
 - 35 dB(A) indoors during the daytime and evening
 - 30 dB(A) indoors during the night-time
- b) background creep in an area or place is prevented or minimised.

State code 23: Wind farm development

SARA is the assessment manager for all wind farm development applications and considers applications against *State code 23: Wind farm development* of the *State Development Assessment Provisions, Version 3.0 (State code 23)*. State code 23 provides the following provisions related to *acoustic amenity*.

Performance Outcome PO10 (Acoustic Amenity Section)

Development is sited and designed to protect the amenity of existing or approved sensitive land uses on non-host lots from acoustic impacts.

Acceptable outcome AO10.1 (Acoustic Amenity Section)

A separation distance of at least 1500 metres is achieved between wind turbines and existing or approved sensitive land uses on non-host lots.

Performance Outcome PO11 (Acoustic Amenity Section)

The predicted acoustic level at all noise affected existing or approved sensitive land uses on **host lots** does not exceed the criteria stated [below as an] outdoor (free-field) night-time (10.00pm to 6.00am) A-weighted equivalent acoustic level (L_{Aeq}):

- 45 dB(A)
- the background noise (L_{A90}) by more than 5 dB(A)
whichever is the greater, for wind speed from cut-in to rated power of the wind turbine and each integer wind speed in between referenced to hub height.

Performance Outcome PO12 (Acoustic Amenity Section)

The predicted acoustic level at all noise affected existing or approved sensitive land uses on **non-host lots** does not exceed the criteria stated [below as an]:

- a) outdoor (free-field) night-time (10.00pm to 6.00am) A-weighted equivalent acoustic level (L_{Aeq})
 - 35 dB(A)
 - the background noise (L_{A90}) by more than 5 dB(A)
whichever is the greater, for wind speed from cut-in to rated power of the wind turbine and each integer wind speed in between referenced to hub height.
- b) outdoor (free-field) day-time (6.00am to 10.00pm) A-weighted equivalent acoustic level (L_{Aeq})
 - 37dB(A)
 - the background noise (L_{A90}) by more than 5 dB(A)
whichever is the greater, for wind speed from cut-in to rated power of the wind turbine and each integer wind speed in between referenced to hub height.

Project Criteria

The project criteria have been developed to satisfy both the scheme and State code 23.

WTG Noise

A key factor in the Policy (as referenced in the scheme) is to *ensure background creep in an area or place is prevented or minimised*.

Whilst State code 23 provides a stand-alone wind farm assessment method, consideration has been made to the scheme's provisions to arrive at an approach for the wind farm which removes the increase in project criteria with an increase in background noise levels.

This approach will satisfy State code 23 (because it achieves its most stringent requirements) and aligns with the environmental values sought by the Policy, by ensuring that the outdoor A-weighted equivalent noise levels (L_{Aeq}) from the WTGs do not exceed the following *baseline* noise criteria:

- 45dB(A) at **host lots**
- 35dB(A) at **non-host lots**.

Notwithstanding the above, background noise monitoring has also been conducted to document the ambient noise in the environment. The data will assist in the future noise monitoring plan (a post approval requirement of State code 23) and in determining the legislative criteria of State code 23, which consists of a *baseline* level and a *background noise level plus 5 dB(A)* requirement, whichever is the greater. The results of the background noise monitoring are summarised in *Echo Acoustics* report with reference ID "232-5".

In addition, and notwithstanding compliance with the 35 dB(A) criterion, a separation distance of at least 1500 metres will be maintained between WTGs and existing or approved non-host lots in the absence of a Deed of Release.

BESS and Transformer Noise

The most onerous "environmental value" of the Policy for a dwelling to protect against adverse impacts is the indoor (night-time) value of 30 dB(A). This equates to an outdoor level of 45 dB(A) based on a typical noise reduction from outside to inside (with a windows open) of 15 dB(A). This noise reduction is consistent with that applied by the Policy during the day and evening periods.

Although designing ancillary infrastructure to 45 dB(A) would achieve the environmental values of the Policy, the recommended approach is to align with the more stringent wind farm criteria. That is, ensure the outdoor A-weighted equivalent noise levels (L_{Aeq}) from ancillary infrastructure do not exceed:

- 45 dB(A) at **host lots**
- 35 dB(A) at **non-host lots**.

Assessment

WTG Noise

Noise Model

A three-dimensional model of the project WTGs has been developed based on the algorithm provided by *ISO 9613-2:1996 Acoustics – Attenuation of sound during propagation outdoors – Part 2: General method of calculation (ISO 9613-2)*.

ISO 9613-2 specifies a method for predicting noise levels at a distance from a source under meteorological conditions favourable to noise propagation. The algorithm also conservatively assumes that these favourable propagation conditions occur simultaneously from all WTGs to all sensitive land uses.

The model incorporates the following:

- sensitive land uses near the project, with locations and host status as detailed in Table 1
- the cumulative operation of all 170 WTGs, with WTG locations as detailed in Table 2
- topographical ground contours
- inputs detailed below, as specified in the *Planning guidance - State code 23: Wind farm development (State code 23 guidance)*:
 - warranted sound power levels for the candidate WTGs at integer wind speeds
 - 10°C temperature
 - 70% relative humidity
 - 50% acoustically hard ground and 50% acoustically soft ground
 - barrier attenuation of no greater than 2 dB(A)
 - 4m receiver height at each sensitive land use
 - application of a 3 dB(A) correction where a "concave" ground profile exists.

The above State code 23 guidance inputs align with the modelling recommendations of the *Institute of Acoustics (UK) "A Good Practice Guide to the Application of ETSU-R-97 for the Assessment and Rating of Wind Turbine Noise"* (the **Good Practice Guide**).

Table 1 Sensitive Land Use Locations and Host Status

Sensitive Land Use ID	Host	Co-ordinates (MGA Zone 56)		Sensitive Land Use ID	Host	Co-ordinates (MGA Zone 56)		Sensitive Land Use ID	Host	Co-ordinates (MGA Zone 56)	
		Easting	Northing			Easting	Northing			Easting	Northing
H01	Yes	226712	7261091	N1	No	241081	7222943	N10	No	223873	7240911
H02	Yes	231972	7254966	N2	No	241084	7222961	N11	No	224961	7247057
H03	Yes	233035	7252302	N3	No	241142	7223034	N12	No	243374	7248290
H04	Yes	228323	7240131	N4	No	242138	7226929	N13	No	244279	7248463
H05	Yes	241338	7239344	N5	No	229139	7227516	N14	No	244202	7248474
H06	Yes	230793	7237878	N6	No	256173	7239743	N15	No	229624	7250788
H07	Yes	230179	7237247	N7	No	223936	7240879	N16	No	222889	7252442
H08	Yes	231566	7234683	N8	No	223899	7240884	N17	No	234261	7253504
H09	Yes	241083	7229248	N9	No	223901	7240904	N18	No	223824	7256625

Table 2 WTG Locations

WTG ID	Co-ordinates (MGA Zone 56)		WTG ID	Co-ordinates (MGA Zone 56)		WTG ID	Co-ordinates (MGA Zone 56)		WTG ID	Co-ordinates (MGA Zone 56)	
	Easting	Northing		Easting	Northing		Easting	Northing		Easting	Northing
1	237000	7246091	44	248589	7242105	89	249991	7238146	132	234393	7233944
2	238910	7248019	45	237963	7242047	90	247614	7238116	133	252670	7233856
3	238766	7247426	46	233213	7242008	91	246583	7238107	134	237762	7233828
4	236860	7247174	47	236713	7241918	92	243593	7237989	135	242171	7233841
5	233957	7247054	48	235205	7241884	93	237982	7238021	136	240256	7233687
6	238207	7246878	49	239734	7241844	94	241582	7237727	137	239155	7233650
7	237418	7246613	50	250883	7241836	95	249518	7237567	138	241765	7233198
8	234884	7246325	51	244761	7241849	96	242928	7237531	139	236292	7233066
9	234632	7245646	52	231369	7241752	97	234422	7237412	140	252124	7233025
10	233604	7245590	53	247939	7241608	98	233272	7237374	141	250106	7232867
11	237120	7245448	54	232915	7241413	99	250809	7237317	142	240481	7233060
12	235697	7245268	55	238411	7241167	100	245123	7237356	143	239147	7232697
13	237888	7244991	56	245239	7241153	101	247747	7237263	144	237590	7232506
14	236872	7244824	57	251276	7241148	102	239848	7237196	145	252433	7232330
15	234378	7244726	58	231016	7241081	103	238837	7236966	146	250734	7232262
16	235444	7244523	59	247447	7240951	104	246083	7236975	147	240804	7231695
17	246345	7244317	60	239419	7240903	105	241445	7236958	148	251449	7231702
18	237065	7244113	61	237122	7240864	106	235486	7236815	149	252279	7231190
19	238129	7244052	62	234514	7240601	107	244688	7236550	150	239988	7231153
20	234830	7244043	63	245957	7240595	108	240125	7236479	151	249099	7230565
21	233857	7243876	64	235762	7240745	109	243328	7236349	152	246892	7229560
22	246368	7243560	65	238729	7240452	110	247920	7236343	153	238965	7230701
23	240261	7243510	66	247013	7240318	111	233456	7236533	154	245735	7230540
24	236926	7243370	67	239916	7240189	112	236389	7236203	155	250925	7230466
25	238324	7243323	68	236673	7240242	113	251225	7236084	156	240070	7230431
26	235345	7243239	69	249299	7239881	114	232270	7239264	157	247009	7230224
27	234176	7243161	70	234816	7239898	115	238167	7235838	158	249562	7229837
28	232125	7243141	72	247497	7239626	116	242965	7235626	159	248543	7229742
29	245953	7242944	73	239220	7239723	117	250259	7235665	160	239444	7229198
30	229273	7243037	75	250502	7239469	118	237106	7235453	161	233815	7240177
31	240728	7242777	76	248641	7239358	119	246745	7236141	162	232819	7243578
32	237649	7242770	77	238421	7239326	120	249287	7235465	163	226721	7243071
33	247844	7242604	78	235312	7239249	121	251846	7235283	164	231503	7240412
34	251496	7242544	79	227701	7243168	122	244858	7234985	165	239460	7229854
35	236255	7242605	80	250220	7238825	123	243039	7234976	166	250776	7234900
36	239410	7242604	81	239904	7238799	124	246830	7235451	167	240578	7232411
37	230479	7242398	82	237877	7238735	125	236240	7234652	168	238403	7246101
38	250305	7242578	83	245442	7238693	126	234295	7234690	169	241271	7243797
39	233889	7242498	84	243242	7238636	127	252490	7234660	170	237604	7236981
40	227041	7242484	85	248254	7238609	128	235333	7234561	171	246529	7234775
41	231579	7242459	86	235172	7238566	129	239255	7234299	172 ¹	233205	7235867
42	245681	7242247	87	234031	7238155	130	242661	7234370			
43	240539	7242093	88	239423	7238175	131	236693	7234024			

¹ Table 2 references 170 WTGs. The project does not include WTG 71 or WTG 74.

Candidate WTGs

The assessment has been based on the *Vestas V172-7.2MW (PO7200-0S operating mode) without serrated trailing edges* and a 166m hub height.

Sound Power Levels

The sound power levels are based on the original equipment manufacturer (**OEM**) noise level data for integer wind speeds (at hub height) from wind turbine cut-in wind speed to the wind speed of the rated power.

The assessment has been based on one-third octave band data between 6.3 Hz and 16 kHz, which is subject to commercial in confidence provisions imposed by the OEM. The total sound power level data presented in Table 3 provides an indication of the noise generated by the WTG. Where required, the OEM one-third octave band data can be provided (subject to the completion of a non-disclosure agreement).

Table 3 Sound Power Levels

Candidate WTG	Integer Hub Height Wind Speed (m/s)	Total Sound Power Level (dB(A))
Vestas V172-7.2MW (PO7200-0S operating mode) without serrated trailing edges	3	97.8
	4	97.8
	5	98.4
	6	101.8
	7	105.4
	8	108.8
	9 to 15	110.1

The measurement of noise levels and contractual agreements to arrive at warranted sound power levels can introduce variations to the noise data. The noise model incorporates an adjustment (addition) of 2 dB(A) to the total sound power levels in Table 3. This adjustment is understood to be greater (more conservative) than what is typically applied to a *Vestas* WTG but is consistent with the *good practice guide* recommendation for uncertainties which are not expressly specified.

Tonality

The one-third octave band data available for the *Vestas V172-7.2MW* WTG indicates that tonality is not a characteristic of the candidate WTG. As noted above, the one-third octave band data can be accessed subject to completion of a non-disclosure agreement.

The assessment has been made on the basis that the WTG selection will not exhibit tonal characteristics. If the final WTG exhibits tonality, then predicted noise levels will be adjusted in accordance with State code 23 guidance as part of a final noise modelling process.

Final Noise Modelling

Details affecting the predicted noise levels can alter during the design, development, and/or procurement stages to suit site constraints, micro-siting requirements and/or OEM selection. The assessment should be updated to reflect changes which can arise through the design and procurement process, to ensure ongoing compliance of the project with the project criteria.

Predicted Noise Levels

Noise level predictions have been made using the noise model in combination with the inputs and assumptions detailed above. Table 4 provides the predicted noise level at each sensitive land use from the cut-in wind speed to the wind speed at rated power in integer steps. The distance to the closest WTG from each sensitive land use is also provided for comparison with *Acceptable outcome AO10.1*.

Table 4 Vestas V172-7.2MW PO7200-0S operating mode - Predicted Noise Levels

Sensitive Land Use ID	Closest WTG (m)	Criterion	Noise level at hub height integer wind speed (dB(A))						
			3 m/s	4 m/s	5 m/s	6 m/s	7 m/s	8 m/s	9 to 15 m/s
H01	15799	45	9	8	9	13	16	20	21
H02	8163	45	16	15	16	20	24	27	28
H03	5338	45	18	18	18	22	26	29	31
H04	2691	45	25	25	26	30	33	37	38
H05	1542	45	32	32	33	36	40	43	45
H06	2032	45	27	27	28	31	35	39	40
H07	2910	45	25	25	26	29	33	37	38
H08	2031	45	26	26	27	30	34	37	39
H09	1574	45	29	29	30	33	37	40	42
N1	6471	35	16	16	16	20	24	27	29
N2	6455	35	16	16	16	20	24	27	29
N3	6399	35	16	16	16	20	24	27	29
N4	3529	35	22	22	23	26	30	34	35
N5	8306	35	13	13	14	18	21	25	26
N6	5100	35	19	19	20	24	27	31	32
N7	3507	35	19	19	20	23	27	31	32
N8	3537	35	19	19	20	23	27	30	32
N9	3526	35	19	19	20	23	27	30	32
N10	3548	35	19	19	20	23	27	30	32
N11	4365	35	18	18	18	22	26	29	31
N12	4479	35	22	22	22	26	30	33	35
N13	4639	35	21	21	22	25	29	33	34
N14	4683	35	21	21	22	25	29	33	34
N15	5729	35	18	18	19	22	26	30	31
N16	10127	35	13	13	14	18	21	25	26
N17	6581	35	17	17	17	21	25	28	30
N18	13862	35	10	10	11	15	18	22	23

The above predicted noise levels indicate that with the *Vestas V172-7.2MW (PO7200-0S operating mode) without* serrated trailing edges and a 166m hub height as the candidate WTG:

- the 45 dB(A) criterion will be achieved at all **host lots**
- the 35 dB(A) criterion will be achieved at all **non-host lots**

In addition, the proposed layout results in the closest WTG to any **non-host lot** being more than the 1500m requirement of *State code 23 Acceptable outcome AO10.1*.

Based on the above, the project can readily satisfy PO10, AO10.1, PO11, and PO12 in accordance with State code 23.

Noise Prediction Contours

The highest noise prediction contours (hub height wind speed of 9m/s and greater²) for the *Vestas V172-7.2MW* (PO7200-0S operating mode) without serrated trailing edges and a 166m hub height are provided in Appendix A.

BESS and Transformer Noise

Noise Model

A three-dimensional model of the project BESSs and associated transformers has been developed based on the algorithm provided by ISO 9613-2.

ISO 9613-2 specifies a method for predicting noise levels at a distance from a source under meteorological conditions favourable to noise propagation. The algorithm also conservatively assumes that these favourable propagation conditions occur simultaneously from all BESSs and transformers to all sensitive land uses.

The model incorporates the following:

- sensitive land uses near the project, with locations and host status as detailed in Table 1
- topographical ground contours
- 10°C temperature
- 70% relative humidity
- 50% acoustically hard ground and 50% acoustically soft ground
- 3m source height
- 1.5m receiver height at each sensitive land use
- substation locations as detailed in Table 5 below.

Table 5 Substation Locations

Substation ID	Co-ordinates (MGA Zone 56)	
	Easting	Northing
1	235800	7244000
2	236150	7240650
3	238250	7233650
4	247600	7237650

BESS

The project will include up to four BESSs (one at each of the four substations) each with a capacity of up to 250MW / 500 MWh.

The final BESS equipment for the project is yet to be determined and will be confirmed during the detailed design, OEM selection and procurement stages.

² The noise generated from a WTG increases with wind speed and then plateaus at 9m/s. The contours show the highest noise level from the WTGs after this plateau in noise.

Sound Power Levels

Potential BESS equipment has been reviewed and whilst commercial sensitivities preclude identification of the specific models or data, this assessment has been based on a BESS that represents a conservative selection from a noise perspective (highest likely noise level).

A BESS operation will vary in load and usage depending on the time of day and the demand of the electricity network.

An assumed cumulative sound power level of 120 dB(A) is utilised by the assessment for each BESS with a capacity of 250 MW / 500 MWh (one at each of the four substations). This represents continuous full load operation of all BESS components with cooling fans at 100% capacity, and therefore is a conservative assumption, particularly for the night period.

Transformers

The noise predictions have been based on one 300 MVA rated transformer located at each of the four substations.

A sound power level of 101 dB(A) has been assumed for each of the 300 MVA transformers as derived from *Australian Standard 60076.10:2023 Power transformers, Part 10: Determination of sound levels*.

Predicted Noise Levels

Noise level predictions have been made using the noise model in combination with the inputs and assumptions detailed above. The predictions indicate that the noise level for the most conservative potential equipment selection operating at 100% capacity is 23 dB(A) at the closest *sensitive land use*, being host lot H05. The predicted noise level at all other host lots and non-host lots will be less than 20 dB(A).

The noise from the BESSs can exhibit tonal noise characteristics when in close proximity. However, the BESSs will incorporate a large number of individual cooling fans that will operate at different speeds, the effect of which will be to mask any dominant tonal characteristics of any one particular fan. Given the above, tonality is unlikely to be a characteristic in practice, particularly when considered in combination with the distances to the sensitive land uses for the project.

Based on the proposed layout and the representative equipment selections, the BESSs and transformers are expected to easily achieve the project criteria by a significant margin. The noise levels and presence of any tonal noise characteristics will be confirmed for the final equipment selections as they are developed by TED.

Noise Prediction Contours

Noise prediction contours for the BESSs and transformers operating at 100% capacity are provided in Appendix B.

Conclusion

Noise impact assessments predict the noise levels from renewable energy facilities based on established input data and compares those noise levels against specific requirements.

The Theodore Wind Farm noise impact assessment, conducted in accordance with *State code 23: Wind farm development (State code 23)*, considers 170 wind turbine generators with a total installed capacity of 1224 MW, battery energy storage systems with a combined battery storage capacity of 1000 MW / 2000 MWh, and associated transformers.

The assessment determines the Theodore Wind Farm can achieve the allowable noise levels and separation distances required for wind turbine generators by State code 23 and the *State Development Assessment Provisions* at all sensitive land uses.

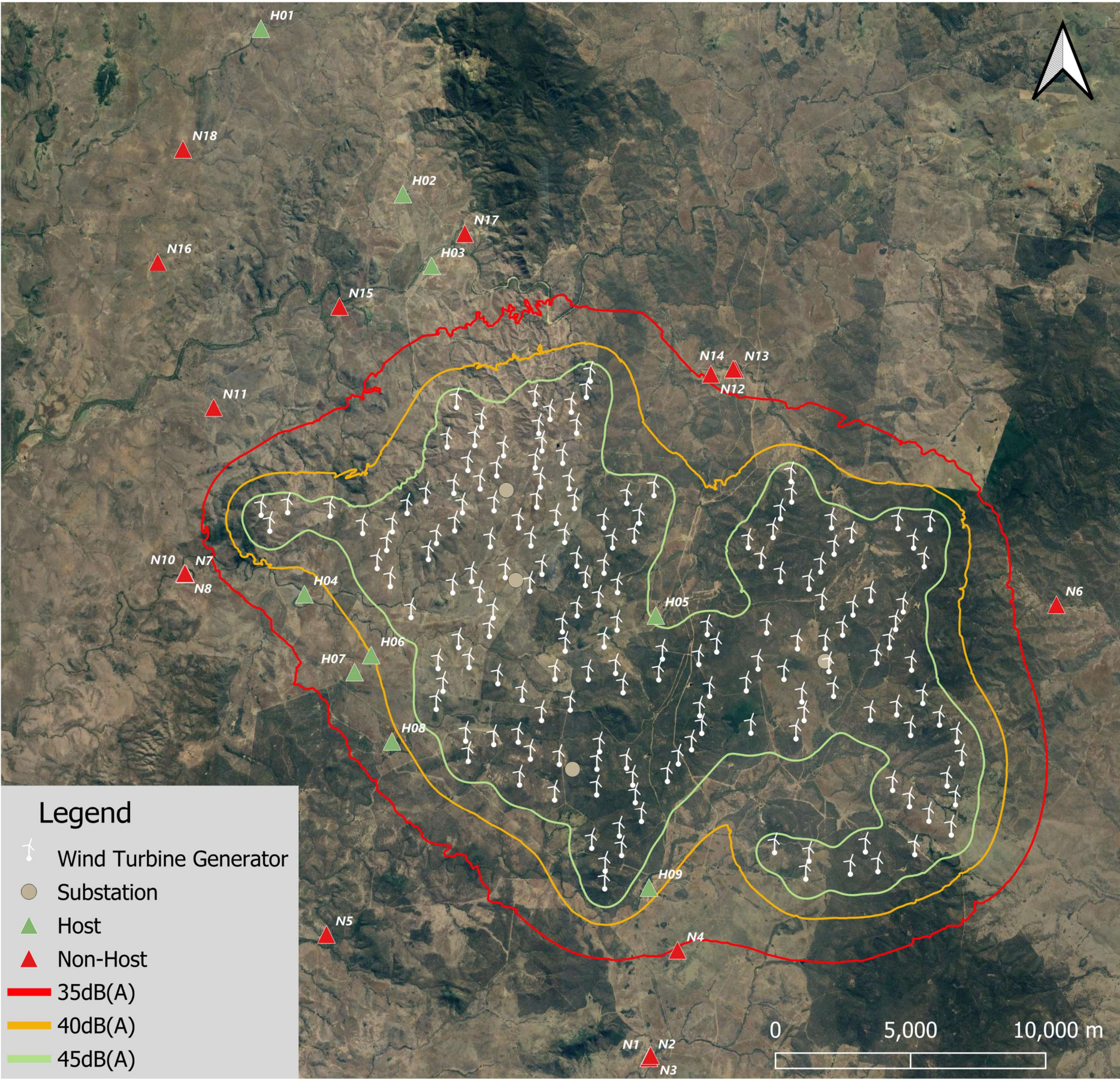
The battery energy storage systems and transformers can achieve the consolidated requirements of the *Environmental Protection (Noise) Policy 2019* to ensure those components do not adversely impact on sensitive land uses.

The assessment confirms the Theodore Wind Farm has been designed to achieve the *baseline* level of State code 23 without reliance on background noise monitoring results.

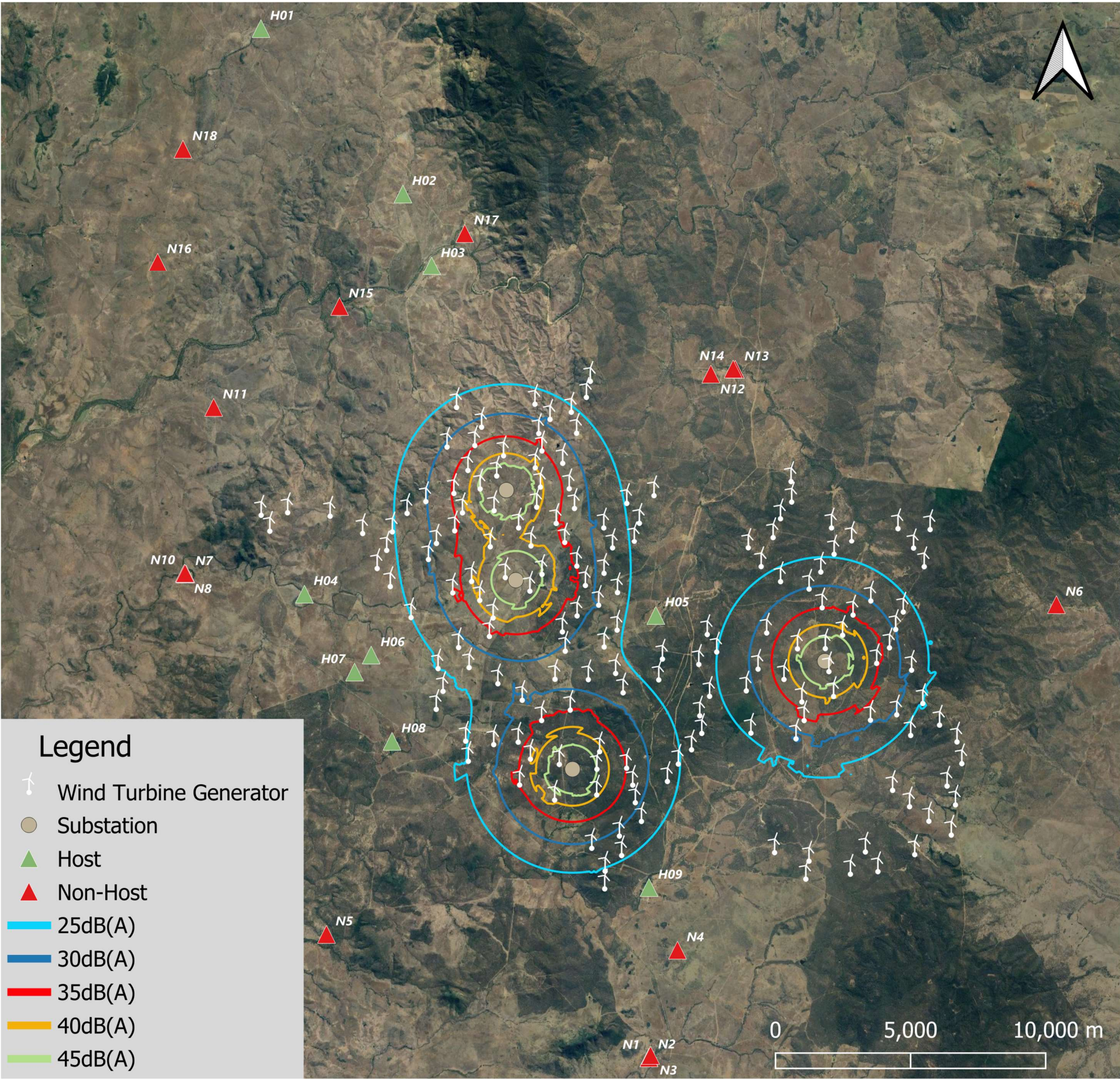
Notwithstanding this design approach, background noise monitoring has been conducted to document the ambient noise in the environment. The data will assist in the future noise monitoring plan (a post approval requirement of State code 23), inform the legislative criteria under State code 23, and provide historical baseline information on the ambient environment should it be required as the project progresses. The results of the background noise monitoring are separately summarised in *Echo Acoustics* report with reference ID "232-5".

Based on the noise impact assessment, the proposed Theodore Wind Farm will satisfy the relevant *State Development Assessment Provisions* and the *Banana Shire Council Planning Scheme* provisions which seek to ensure the project will not unreasonably impact on the acoustic amenity of existing or approved sensitive land uses.

Appendix A: WTG Noise Prediction Contour



Appendix B: BESS and Transformer Noise Prediction Contour



References

- Australian Standard 60076.10:2023 Power transformers, Part 10: Determination of sound levels*
- Banana Shire Council Planning Scheme 2021*
- Environmental Protection Act 1994*
- Environmental Protection (Noise) Policy 2019*
- Environmental Protection (Noise) Policy 2019 - Explanatory notes for SL 2019 No. 154 made under the Environmental Protection Act 1994*
- Institute of Acoustics (UK) "A Good Practice Guide to the Application of ETSU-R-97 for the Assessment and Rating of Wind Turbine Noise", 2013*
- ISO 9613-2:1996 Acoustics – Attenuation of sound during propagation outdoors – Part 2: General method of calculation*
- Planning guidance - State code 23: Wind farm development February 2022*
- State code 23: Wind farm development of the State Development Assessment Provision, Version 3.0, February 2022*
- Vestas Power Solutions - Third octave noise emission EnVentus™ V172-7.2MW – (restricted) Document no 0128-4336_00, dated 30 June 2022*

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